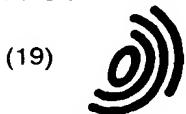


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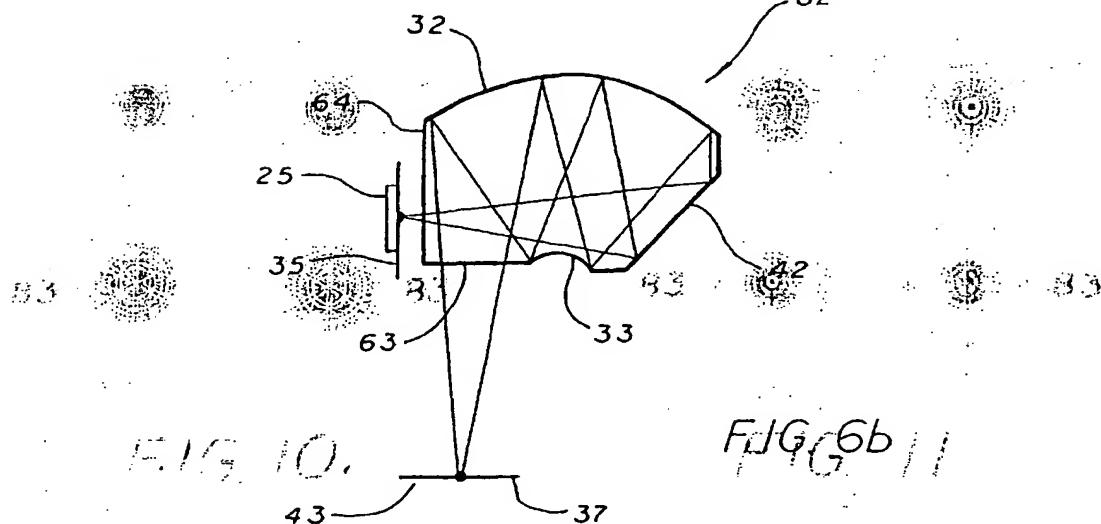
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### (54) Scanning system

(57) In a system for scanning a document (43), a light source (22) illuminates the document; an imager (24, 41, 41', 61, 62) receives light from the document and directs it toward a detector array (25) which produces a corresponding array of electrical signals. The imager has several optical properties that are useful either individually or in combination. The imager is telecentric and thereby ensures that image size and magnification are insensitive to object displacement along the optical axis (46, 46') and image brightness is uniform independent of object off-axis distance. An aspheric element (33) within the imager balances focus variation (82-81-83)

within the depth of field with spherical aberration and thereby provide nearly uniform image resolution. A diffraction pattern (33') carried by the imager, corrects for spectral dispersion which occurs when light passes (63) from air into a refractive material (61, 62). An imager with a reflecting surface (32, 33) provides a system that is subject to little or no chromatic aberration. A solid imager (61, 62) with multiple internal reflecting surfaces (32, 33, 42) in optical series (32-33-32-42), configured to include the previously mentioned optical properties, also provides for highly stable alignment of reflecting surfaces.



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**Description**

This invention relates generally to systems for scanning documents, and more specifically to a system employing particular types of imagers for a swath scanning system.

Throughout this document the term imager refers to an optical device or system for receiving light from an object and directing light to an image. The phrase swath scanning system refers to a scanning system that serially acquires successive swaths of a document; such a system thus differs from a scanner that employs a linear detector array, fully extended across the document, to acquire entire pixel rows one at a time.

In a pixel-based scanner, printer, copier, or fax machine, a swath consists of a number of pixel lines, modernly on the order of twenty to two hundred. In a swath scanning system the pixel columns within each swath are serially acquired, one pixel column at a time, by an imager and detector array which move together across the document on a carriage.

This type of operation may be referred to as "carriage scanning", "swath scanning", or "swath-type scanning", and the devices "carriage scanners", "swath scanners", or "swath-type scanners". They are also sometimes called "moving scanners".

The ability of any scanning system to reproduce a document is largely dependent on the performance of its imager. The typical prior art imager used in a document scanning system is purely refractive, aside from a planar folding mirror, and usually consists of a simple single lens or in some cases a compound lens system. Several optical characteristics useful in evaluating an imager's performance are set forth below.

(b) Focus and resolution - Imager focus varies as a function of object location, axially, within the imager's depth of field. A typical prior art refractive imager has excellent focus near the center of the depth of field which decreases to merely acceptable focus behind and in front of that best-focus position, or in other words, near the ends of the depth of field.

Closely associated with focus is resolution. Resolution is a quantitative measure of an optical system's ability to produce a sharp image of an object. Imager resolution is affected by the quality of focus and, as will be seen, optical aberrations such as chromatic aberration. An imager with poor focus has poor or coarse resolution; an imager with good focus has good or fine resolution.

When points of an object are at different locations within a typical refractive imager's depth of field, i.e., at different axial positions, the object rays from points near the center of the depth of field are better focused in the resulting image than points farther from the center of the field. In scanning, variations in depth of field location arise when the document being scanned is wrinkled or misfed. The result is an image with varying focus; it is defocused at points where wrinkling has displaced the document from the best focal position.

Such a defect is particularly conspicuous when the document carries lines or edges angled very shallowly to the pixel grid so that serious aliasing occurs. Aliasing is smoothed out in areas that are defocused but appears plainly where the document is in sharp focus, an appearance that is both unpleasant and baffling to the casual user.

Therefore, it is disadvantageous to use a conventional scanner imager that produces images with variable resolution, dependent on axial displacement of the object within the imager's depth of field.

(c) Distortion - Distortion arises from variation of magnification due to (1) off-axis distance of an object point in a document, and (2) axial displacement of the document. A typical prior art refractive imager is subject to significant distortion from both of these causes.

Variation of magnification with axial position arises because the primary ray from each object point is angled to the optical axis. Therefore fluttering or crumpling of a document, displacing any small region of the document in and out along the optical path, changes the off-axis distance of the intercept of the angled primary ray with the document surface. This change in off-axis distance amounts, for that region of the document, to variation in magnification, i.e., distortion.

It is thus disadvantageous to use a conventional scanner imager that produces images which are distorted when documents are wrinkled, dependent upon both off-axis distance and axial displacement of an object.

(d) Brightness - Image brightness varies as a function of object off-axis distance. A typical prior art refractive imager collects more light from object points closer to the imager's optical axis than from points farther away from the axis.

The result is a swath image with a bright midregion and relatively dark extremes, producing a mottled or dirty effect. It is therefore disadvantageous to use a conventional scanner imager that collects light nonuniformly, dependent upon object off-axis distance.

(e) Chromatic aberration - In a typical prior art refractive imager, chromatic aberration occurs when an object ray of white light refracts through the optical material of the imager. This refraction causes rays of various wavelengths to leave the material at different angles (spectral dispersion) and come into focus as points of different colors at different locations.

The result is a blurred image. The amount of blur is greater for object points farther from the optical axis because their rays enter the imager at its extremes, where refraction is typically greater, thus again creating a patchwork effect,

or an overall impression of variable quality in finished copies. Accordingly, it is disadvantageous to use a conventional scanner imager with significant chromatic aberration.

(f) Banding - The above-discussed effects, in a swath scanner, both individually or collectively result in undesirable conspicuous banding. This occurs as follows.

Suppose an imager is called upon to scan a document composed of a series of closely spaced horizontal lines. Further suppose the imager has nonuniform brightness, chromatic aberration, and expansive distortion. Under these conditions each swath produced by the imager has dark, blurred, expansively spaced lines at the top and bottom of the swath, and bright, clear, narrowly spaced lines in the midregion of the swath.

Upon reassembly of the swaths a banding effect is apparent. The document image is a cyclic display of dark, blurred, expansively spaced groups of lines alternating with bright, clear, narrowly spaced groups of lines.

The magnitude of these effects depends on the size of the swath. The bigger the swath, the farther points are from the imager's optical axis; accordingly, there is greater distortion at the extremes, greater disparity between the brightness of the swath center and the swath edge, and greater blur at the extremes.

(g) Inefficient light collection - An imager having inefficient light collection capability does not collect adequate light from the object. This results in an image with poor contrast.

In a scanning system, sufficient light must be collected from each pixel being scanned. This is particularly important in a swath scanning system because the rate at which each pixel is acquired is proportionately higher relative to a full transverse scanner. Therefore, it is disadvantageous to use a conventional scanner imager that cannot collect enough light from each pixel during the shorter exposure times needed for swath scanning.

(h) Related devices - As previously mentioned, a typical scanning system employs, as its imager, a single refractive lens or a compound lens system. A single lens does not possess the desired characteristics. The image quality of a single lens is strongly dependent on both off-axis distance and axial displacement of an object.

A complex, compound refractive lens system has some of the desired characteristics because it can correct for some off-axis distance effects such as distortion and chromatic aberration. This type of system, however, is moderately expensive and delicate. Considering the commercial and industrial environments in which these imagers must operate, it is disadvantageous to use an imager that is costly or sensitive.

Besides the imager, other elements of a scanning system may compensate for poor imager performance. For example, the detector array may be calibrated to compensate for brightness variation. Compensation for inefficient light collection may be obtained by slowing down the scanning rate, thereby increasing exposure time, or by increasing the level of object illumination.

These solutions, while compensating for the inadequacies of the imager, create other problems. A calibrated detector array requires application of a weighting factor for each row in a swath, and a sizable calibration can use up some of the effective dynamic range, thereby degrading effective signal-to-noise ratio. Slower scanning speed results in a less efficient scanner, and greater illumination requires more operating power.

(i) Previously unrelated devices - Not previously associated with or suggested for use in scanners, are certain devices which have useful optical properties. Dating from Isaac Newton's astronomical telescope, it has been known to use nonrefracting, or reflecting, elements in imaging devices. Benefits of simple reflecting imagers include reduced chromatic aberration and increased light efficiency.

More modern imaging devices, such as the Dyson catadioptric imager and the Offner catoptric imager, have further useful optical properties. The Dyson imager has low distortion (near uniform magnification); however, it cannot correct for poor resolution due to axial displacement of an object within the imager's depth of field.

The original Offner imager, never suggested for use in a scanner, combines favorable features of reflecting imagers and the Dyson imager. It can accommodate axial displacement of an object in terms of magnification uniformity, but not in terms of resolution uniformity. In other words, the original Offner imager cannot produce an image with uniform resolution within its depth of field.

As previously stated, none of these imaging devices has been associated with, or suggested for use in, document scanning systems.

Thus important aspects of the technology used in the field of the invention remain amenable to useful refinement.

The present invention seeks to provide an improved system for scanning documents.

According to one aspect of the present invention, there is provided a system for scanning a document as specified in claim 1.

In preferred embodiments, the scanning system includes a telecentric imager for receiving light from the document and directing the light toward the detector array.

In particular the telecentric imager ensures that magnification and image size are insensitive to axial displacement of the object within the imager's depth of field, in other words, nearly distortion free. Telecentricity also inherently provides uniform light collection independent of object distance off the optical axis; the result is an image with uniform brightness.

In a second preferred embodiment, the scanning system comprises an optical axis, the document is subject to

axial displacement, and an imager for receiving light from the document and directing the light towards the detector array.

The imager preferably includes an aspheric element for introducing spherical aberration to reduce variation of resolution as a function of axial displacement.

In particular the aspheric element introduces spherical aberration into the imager to provide more uniform resolution independent of axial displacement of the object (due to a wrinkled or misfed document) within the imager's depth of field.

It is preferred that the aspheric element be located at an aperture stop of the system. It is also desirable that the imager be telecentric.

It is further desirable that the imager include plural surfaces in optical series, and that one or more of the surfaces carry a diffraction pattern to correct spectral dispersion caused by refraction at one of the surfaces.

In another preferred embodiment, the scanning system includes an imager, having plural surfaces in optical series, for receiving light from the document and directing the light toward the detector array. It also has a diffraction pattern, carried by one or more of the surfaces, for correcting spectral dispersion caused by refraction at one of the surfaces.

In particular, the diffraction pattern corrects spectral dispersion which occurs when light passes from air into a refractive material. The diffraction pattern cancels the spectral dispersion by causing the light to disperse in a direction, equal but opposite, to the refractive dispersion, thereby greatly reducing image blur. Again, it is desirable that the imager be telecentric.

As to preferred embodiments of a fourth type, the system can further include a reflecting imager for receiving light from the document and directing the light toward the detector array. The imager is, for example, one that obtains optical power at a reflecting surface rather than through a lens, i.e., one whose focal elements are reflectors.

Such an arrangement aims to provide a system that is subject to little or no chromatic aberration, as will be seen, it is preferably practiced in conjunction with certain other features or characteristics.

For example, it is preferred that the reflecting imager comprise plural mirrors aligned in optical series. It is also desirable that the plural mirrors comprise converging mirror means and a diverging mirror. The phrase "mirror means" is meant to encompass a plurality of mirrors, as well as a single mirror. Generally, a converging mirror means is a mirror that causes rays of light parallel to its axis to converge. A diverging mirror is typically thought of as a concave mirror (or a positive mirror) that causes rays of light parallel to its axis to diverge.

Throughout this document, regardless of the concave or convex appearance of a mirror, the terms converging and diverging will be used to describe the properties of a mirror. For example, it will be seen that in certain solid-optical-block embodiments the converging mirror is, when viewed from the exterior of the solid, convex in shape; however, when viewed from the interior of the solid it is concave. Therefore, to avoid confusion the terms concave and convex will be avoided as objects being referred along the optical axis.

It is further desirable that the diverging mirror be positioned to receive light from the converging mirror means and reflect the light back toward the converging mirror means. It is still further desirable to have a third mirror positioned in optical series with the converging mirror means to fold the optical path.

It is also preferred that the reflecting imager be a solid optical material having an internal reflective surface. The imager may also have plural internal reflecting surfaces in optical series.

It is also desirable that the solid optical material define internal converging mirror means and an internal diverging mirror. The previously introduced features concerning the position of the diverging mirror and the inclusion of a third mirror are also desirable in the solid-optical-material imager.

It is furthermore preferred that the optical axis of the diverging mirror be aligned with the optical axis of the converging mirror means.

It is also desirable that the diverging mirror be slightly aspheric for reducing variation of resolution, as previously mentioned. It is further desirable that the diverging mirror carry a diffraction pattern to compensate for chromatic aberration caused by refraction at the air/surface interface, also mentioned previously.

Additionally, it is preferred that the scanning system have means for translating the detector array and the imager together across the document to obtain a signal array representing a swath of the document.

As to preferred embodiments of a fifth type, a system further includes an imager made of a solid optical material that defines internal converging mirror means and an aspheric internal diverging mirror. The diverging mirror is positioned to receive light from the converging mirror means, and to reflect the light toward the converging mirror means.

The system still further includes a carriage for translating the detector array and imager together across the document to obtain a signal array representing a swath of the document.

The solid configuration aims to provide for highly stable alignment, a feature particularly beneficial to systems used in commercial or industrial settings, and its carriage provides a mechanism for moving the imager and detector array across the document, thereby enabling the use of compact inexpensive lighting, optics and detectors in acquiring a full-page image. Nevertheless it is again preferably practiced in conjunction with certain other features or characteristics.

For example, it is preferred that the solid optical material further define a third internal mirror positioned to receive light from the converging mirror means and fold the light toward the detector array. It is also desirable that the carriage translate the illuminating means, and that the diverging mirror carry a diffraction pattern.

Embodiments of the present invention will now be described, by way of example only, with reference to the accompanying drawings, of which:

- Fig. 1 is a front elevation of a preferred embodiment of the invention that includes a carriage holding two pens, and also holding a sensor assembly with its cover in place;
  - Fig. 2 is a front elevation of the sensor assembly of Fig. 1 with its cover removed;
  - Fig. 3 is a diagram, in longitudinal section in a system plane of symmetry, after Kingsdale, Lens Design Fundamentals (1978), showing very schematically an imaging optical train attributed to A. Offner;
  - Fig. 4a is a plan of a document showing a swath and an instantaneous field of view;
  - Figs. 4b and 4c are diagrams, in longitudinal section in a system plane of symmetry, very schematically showing preferred imaging optical trains that fold the optical path and that generally speaking can be used in the Fig. 1 and 2 embodiment, and in particular illustrating in Fig. 4b alignment of the system plane of symmetry with a desired field of view in an object, and in Fig. 4c perpendicularity of the same plane and field;
  - Fig. 5 is a three-dimensional representation of light flow through embodiments similar to the ones shown in Figs. 4b and 4c;
  - Figs. 6a and 6b are schematic diagrams, in longitudinal section in a system plane of symmetry, showing preferred imaging optical paths inside a solid block of material, usable in the Fig. 1 and 2 embodiment, the imager in Fig. 6a being unfolded, and that in Fig. 6b being folded;
  - Fig. 6c shows a diffraction pattern carried by the imagers of Figs. 6a and 6b;
  - Fig. 7 is a three-dimensional representation of light flow through the imager shown in Fig. 6b;
  - Fig. 8 is a longitudinal section of light rays along the optical axis in a system without spherical aberration, and showing strongly varying sharpness along the optical axis;
  - Fig. 9 is a like view of light rays along the optical axis in a system with added spherical aberration, and showing reduced variation of sharpness along the optical axis;
  - Fig. 10 is a cross-sectional ray-spot diagram corresponding to Fig. 8;
  - Fig. 11 is a like view but corresponding to Fig. 9;
  - Fig. 12a is an isometric or perspective representation of the imager of Figs. 2 and 6b, taken from below-right; and
  - Figs. 12b through 12e are orthographic views of the imager of Fig. 12a: Fig. 12b is a left elevation showing the exit face; Fig. 12c a front elevation; Fig. 12d a right elevation, and Fig. 12e a bottom plan showing the entry face.
- As shown in Fig. 1, preferred embodiments of the invention may be advantageously incorporated into a device having a carriage 11 such as typically associated with an automatic printer, as for instance a thermal-inkjet desktop printer sensitive to lateral displacement along the optical axis. This combination is a particularly powerful one, since much of the necessary mechanics, electronics and firmware for scanning are already present in such a printer. Scanning functions therefore can be added at extremely modest direct cost.

The carriage 11 holds a black pen cartridge 12 and a color pen cartridge 13. Also securely mounted to the carriage 11 is a sensor assembly 14, shown with its cover 15 in place.

Internal elements of a preferred sensor assembly 14 include a housing 21 (Fig. 2) with plural bays 23 for holding light-emitting diodes (LEDs) 22. An LED 22 should be installed in each bay 23. The housing 21 also has a channel 26 for passage of incoming light from a document (not shown) below the assembly 14.

Mounted in the housing 21 is an imager 24, shown here in the form of a solid optical block whose surfaces define curved internal mirrors and a planar folding mirror. The solid-block embodiment with a folding mirror, or for shorthand purposes "solid-fold imager" is merely one of several embodiments which can effectively function within the sensor assembly 14. The housing 21 further contains a detector array 25.

Imager 24 is positioned to receive light, through channel 26, from the document being scanned and to direct the light toward the detector array 25. In this embodiment the imager forms, at the detector array 25, an image of document objects located in the imager's field of view. Detector array 25 responds to the light it receives by producing a corresponding array of electrical signals which it forwards to system electronics (not shown) for storage.

The original Offner imager 31 (Fig. 3) does not employ a solid block to define internal mirrors; rather the imager has mirrors formed to receive and redirect light that passes through the air. This original Offner imager will be abbreviated "air imager". The air imager 31 includes converging mirror means 32 and a diverging mirror 33.

Rays 38, 39 from an object point 34 in an object plane 37 are collected by the converging mirror means 32 and directed toward the diverging mirror 33. The diverging mirror 33 in turn redirects the rays 48, 49 back toward the converging mirror means 32, which once again redirects the rays toward an image plane 35 to form an image point

36. Note that the object plane 37 and the image plane 35 are coplanar, making this embodiment of the air imager 31 symmetric.

For optimum imager performance, in this embodiment and other embodiments, it is desirable to position the aperture stop of the imager at the imager's focal point. In this embodiment the diverging mirror 33, i.e. the aperture stop, is located at the focal point midway between converging mirror means 32 and the object plane 37.

Placement of the diverging mirror 33 in this location makes the imager telecentric. This means that principal rays to each image point are closely parallel to the optical axis, so that image magnification and size are insensitive to axial displacement, essentially eliminating distortion.

TELECENTRICITY IS RELEVANT

This characteristic results in images with uniform brightness.

Figs. 4b and 4c depict an air-fold imager 41. Like the air imager 31, the air-fold imager 41 includes converging mirror means 32 and a diverging mirror 33. The distinction between the air imager 31 and the air-fold imager 41 is the addition of a planar folding mirror 42. The function of the folding mirror 42 is to fold the optical path away from the document 43 toward the detector array 25.

The folding of the optical path is better appreciated upon viewing Fig. 5, which depicts, three dimensionally, the reflection of light through the air-fold imager 41'. The path is identical to that of the air-imager 41 except that the folding mirror 42 rotates the exit beam ninety degrees. From Fig. 5 it is apparent that the converging mirror means 32 may be sliced, e.g. fore-and-aft parallel to a diameter, into two mirrors without disturbing the flow of light. The converging mirror means 32 may be further sectioned, if desired, in other ways with moderate light loss. Accordingly, converging mirror means 32 may be one mirror or plural mirrors.

While not necessary for imager functionality, the folding mirror 42 is beneficial from a mechanical design perspective because it directs the light away from the document 43. As can be seen in Figs. 4b and 4c, this enables placement of the detector array 25 where the array does not interfere with the document 43, while still providing a symmetrical imager.

Figs. 4b and 4c further depict two configurations of a scanning system using the air-fold imager 41. It is to be understood that as far as these two configurations are concerned, any one of various embodiments of the imager may be substituted for the air-fold imager 41. The distinction between the configurations lies in the orientation of the air-fold imager 41 relative to the document 43, and more particularly to the instantaneous field of view (IFOV) 45.

In Fig. 4a, document 43 shows a swath 44, one of a series of such swaths arranged along the length of the paper. Contained within each swath 44, is an IFOV 45, which is typically a one pixel column of the swath 44. The IFOV 45 is the portion of the swath 44 that is being imaged at a given instant.

Figs. 4a and 4b considered together illustrate a first configuration: the IFOV 45 lies within the plane of symmetry of the air-fold imager 41. As shown, however, all object points are at a considerable distance off the system axis 46 of the air-fold imager 41. Even points at the bottom of the IFOV 45 are above, though close to, the system axis 46. This distance increases greatly for points farther up the IFOV. This off-system-axis distance degrades imaging performance (particularly for a solid version of the imager as discussed below). The imager of Fig. 4b is drawn in the same orientation as the imager of Fig. 3.

Fig. 4a and 4c considered together depict a second configuration. In this preferred configuration, the IFOV 45 runs in and out of the plane of the paper. It is orthogonal to the plane of symmetry of the air-fold imager. All object points in the IFOV 45 are more nearly equidistant from the imaging system axis 46'. This maintains best available imaging. The imager in Fig. 4c is identical to that of Fig. 4b, but now can be seen in the same orientation as the imager in Fig. 2.

Fig. 6a shows a solid imager 61 while Fig. 6b shows a solid-fold imager 62. Each solid imager 61, 62 is made of solid optical material that forms internal converging mirror means 32 and diverging mirror 33. In the solid-fold imager 62, the addition of an interior folding mirror 42 redirects the light. These solid imagers 61, 62 share features of the previously discussed air imager counterparts.

Fig. 7 is a three dimensional rendering of a light path through a solid-fold imager 62. As the drawing suggests, the converging mirror means 32 may be split across the middle without disturbing the flow of light.

An advantage of solid imagers 61, 62 is the assurance of stable axial alignment of the converging mirror means 32 and the diverging mirror 33 through precision mold fabrication. Through mold fabrication the mechanical alignment problems associated with multiple mirror systems are avoided.

The solid imager, however, is more susceptible to off-optical-axis image degradation, particularly due to chromatic aberration; although this can be largely corrected by diffraction as described later in this document. Hence the second configuration of Fig. 4c may be particularly desirable for solid imagers.

Advantages of air imagers over solid imagers also include reduced material (there is no solid optical material between the mirrors) and consequently decreased mold cycle time, both resulting in lower cost. The air imager and solid imager are equally effective. The preferred embodiment at present is the solid imager; however, the air imager is being considered for future use.

It should be noted that symmetry, while desirable, is not absolutely necessary. To keep the sensor assembly housing 21 and thus the overall product enclosure as narrow as possible, it is desirable to keep the detector array 25 as close

as possible to the system axis. In the solid-fold equivalent of the Fig. 4c orientation the exit surface 64 protrudes at the left side of the sensor assembly 14, and I prefer to narrow the optical block to reduce this width.

Another desirable adjustment to the optical path is increasing the distance between the object plane 37 and the front surface 63. A principal benefit of moving the object plane 37 farther from the front surface 63 is better object illumination. Light can be aimed at the document from farther back, resulting in more uniform illumination.

As an example of such adjustments, the object plane 37, originally at a distance of approximately 13 mm from the front surface 63, was moved to a distance of approximately 22 mm. The image plane 35, while approximately 13 mm from the front surface 63, was placed roughly 2 mm from the top surface 64.

Interestingly, the long object path in principle can be exploited to eliminate the folding mirror 42 if desired. With clearance of more than 2 cm, the detector array 25 could be placed between the imager and the document. Suitable protection of the detector array 25 should be provided, or the document path curved to add additional clearance.

An important feature of all preferred embodiments of the imager is the ability to produce images with roughly uniform resolution regardless of object displacement along the optical axis of the imager. In the scanning context this type of displacement is usually caused by a wrinkled or misfed document.

Nearly constant resolution is obtained by purposely introducing an aspheric element into an imager that is otherwise free of spherical aberration. Figs. 8 and 10 show rays converging at a common point near the focal plane 81. This type of longitudinal ray pattern occurs when the system is free of spherical aberration.

Fig. 10 depicts a series of ray-scatter patterns at various points along the optical axis between the first extreme 82 of the depth of field and the second extreme 83. It is shown that the patterns vary in size, with the smallest circle 84 occurring at (or defining) the nominal focal plane 81 of the imager.

Figs. 9 and 11 (corresponding to Figs. 8 and 10 respectively) illustrate like rays in an optical system having slight spherical aberration. The result is a group of rays which maintain a slight scatter throughout the nominal focal region.

As illustrated in Fig. 11, spherical aberration, introduced into the imager through the addition of an aspheric element, causes the image to be relatively blurred in regions where it would otherwise be in sharper focus. This blurring effect, in combination with the conventional defocus effect of Figs. 8 and 10, results in an image with nearly constant resolution along the imager's depth of field, from first extreme 82 to second extreme 83. Comparing Figs. 10 and 11, the addition of an aspheric element has little effect on the images near the extremes 82, 83; 82', 83' of the depth of field; the blur is only slightly wider. Near the focal planes 81, 81', however, the difference between the images is apparent, with the aspheric element causing the image to be scattered, significantly more so than the image without spherical aberration. The result is more-nearly uniform resolution within the depth of field. Some sacrifice in fineness of resolution at the nominal focus accompanies this improvement in uniformity, as will be evident from the illustrations. An imager of this type, however, inherently has extraordinarily fine resolution; hence some deliberate degradation is acceptable for this purpose.

The aspheric element is preferably introduced at the aperture stop of the imager; this positioning ensures that light from all points in the object will be treated consistently. The result, in particular, is that the above-described axial elongation of the focal point or circle, to, in essence, nearly a focal cylinder, is reasonably uniform for off-axis, on-axis and moderate skew rays. Otherwise, some residual banding, seen as periodic blur variation, could remain due to interaction between axial dependence of resolution and position of object details within the field of view. For those skilled in the art, an aspheric diverging mirror 33 is readily designed using a ray tracing program such as CodeV (from Optical Research Associates) or Zemax (from Focus Software), in the following manner.

The worst-case focus within tolerance is determined for a spherical diverging mirror. The marginal transverse ray aberration is then calculated for the worst-case-focus situation. The conic constant for the diverging mirror surface is then chosen so that the difference between the marginal transverse ray aberration and the largest zonal transverse ray aberration is approximately one-half the previously calculated defocused aberration of the spherical system. The curvature and conic constant are then optimized using the ray tracing program. Higher order terms of aspheric surface figures can be used in addition to the conic constant. The imager mold, from which solid imagers will be cast, is machine formed to include the aspheric diverging mirror 33 characteristics, as determined by the software.

Although the previous discussion of an aspheric element centered around its use in the solid-fold imager, this feature is equally applicable to all imager embodiments disclosed herein.

The use of a solid optical material in the imager introduces slight spectral dispersion, i.e., slight chromatic aberration, into the imager. The dispersion occurs as light rays enter and leave the solid optical material at its planar surfaces 63, 64. If left uncorrected this effect will result in a blurred image.

To compensate for this refractive effect it is desirable that the imager carry a diffraction pattern 33', as illustrated in Fig. 6c. The diffraction pattern 33' generates dispersion that is equal and opposite to the refractive dispersion occurring at the air/solid interfaces, thereby canceling the refractive dispersion. It is important to note that at different levels it is preferable to introduce the diffraction pattern 33' at the aperture stop of the imager. For example, in the imager of Fig. 6c the diffraction pattern 33' is carried by diverging mirror 33. A model of the diffraction pattern 33' is determined with the aid of a ray tracing program, such as those previously mentioned. This model is used to predict the effect.

The diffraction pattern 33' will change the diverging power at the nominal wavelength of the diverging mirror 33. As a result, the curvature of the diverging mirror 33 must be altered so the total diverging power of the diffractive diverging mirror remains the same as that for a nondiffractive diverging mirror.

Like the previously discussed aspheric element, the diffraction pattern 33' and accompanying surface curvature modification are introduced into the imager during fabrication. Through numerically controlled machining processes the diffraction pattern 33' is diamond tooled into a mold, preferably made of nickel-coated stainless steel, from which numerous imagers are to be cast.

Fig. 12 shows detail views of a solid-fold imager 62. The solid-fold imager 62 is made of optical quality acrylic which is formed to define the converging mirror 32 in the top face; diverging mirror 33 and object window 132 in the bottom, entry face 63; image window 131 in the left side, exit face 64; right side face 121; front face 122, rear face 123, and folding mirror 42 bridging the right side and bottom faces 121, 63. Except for the converging and diverging mirrors 32, 33, all surfaces are planar.

The exit window 131 in the left face 64 passes to the detector array the light received from the folding mirror 42. To reduce stray light, the top surface 64 is blackened, except for the detector array window 131.

To reduce stray light, the front surface 63 is blackened except for the object window 132, and the left side surface 122, right side surface 123, and bottom surface 121 are also blackened.

The diverging mirror 33 and converging mirror 32 are mirror coated for ninety-three percent minimum internal reflection across the visible spectrum. After application of the mirror coatings the backs of the coatings may be blackened. The angle formed at the intersection of front surface 63 and folding mirror 42 is forty-five degrees.

Other specifications of the solid-fold imager 62 as explained above, include these approximate values:

MILLIMETERS	DIMENSION
25	6.0 distance from centerline 141 to bottom edge of detector window 131
25	6.0 distance from centerline 141 to top edge of detector window 131
25	17.8 distance from apex of converging mirror 32 to remote edge of detector window 131
30	16.2 distance from apex of converging mirror 32 to near edge of detector window 131
30	7.9 distance from diverging mirror horizontal centerline 142 to top of object window 132
30	4.1 distance from diverging mirror horizontal centerline 142 to bottom of object window 132
30	2.89 distance from diverging mirror horizontal centerline 142 to top of folding mirror 42
30	10.00 distance from diverging mirror vertical centerline 143 to left side 122
30	20.00 distance from left side 122 to right side 123
35	4.4 diameter of diverging mirror 33
35	40.45 radius of curvature of converging mirror 32
35	20.12 distance from apex of converging mirror 32 to front surface 124
35	12.00 distance from apex of converging mirror 32 to remote edge of bottom surface 121
35	22.00 distance from top surface 64 to bottom surface 121
40	21.36 distance from front surface 124 to the nominal document plane 133
40	21.47 radius of curvature of diverging mirror 33

For preferred imagers disclosed in this document, the relationship between the converging mirror means 32' and the diverging mirror 33, and the relationship between the imager and the object plane 37' and the image plane 35, may be generalized as follows:

Given the distance  $m$  between the converging mirror means 32' and the diverging mirror 33, the converging mirror means 32' have a radius of curvature roughly equal to  $2m$ . The diverging mirror 33 has a radius of curvature roughly equal to  $m$ .

Referring to Fig. 3, for the air imager 31, the distance  $d$  from the object plane 35 to the nominal front plane 40 and the distance  $s$  from the nominal front plane 40 to the image plane 37' satisfy the relation:

$$d + s = 2m$$

The original air imager 31 is not a solid block, but a folded mirror, under the imager.

Referring to Fig. 6a, for the solid imager 61,  $d$  is the distance from the object plane 35 to the front surface 63 and  $s$  is the distance from the front surface 63 to the image plane 37'. Where  $n$  is the index of refraction of the optical material, the distances  $d$  and  $s$  roughly satisfy the relation:

$$\frac{d}{n} + s = 2m$$

$$d + s \geq 2m/n.$$

For fold-imagers 41, 62, the distances and radii of curvature are calculated as for unfolded imagers 31, 61 respectively, with the fold being added afterward. The distances and radii of curvature given above are only applicable for a very rough first-order design. The parameters are subsequently optimized for higher-order image quality using an optimizing ray-tracing software program, such as those previously mentioned.

The preferred embodiment is a scanning system generally intended for use in a scanner; however, it may also be used in a printer, copier, FAX machine, or other related device.

The disclosures in United States patent application no. 08/665,777, from which this application claims priority, and in the abstract accompanying this application are incorporated herein by reference. The disclosure of the prior application relates to a decorative pattern for a floor covering material, the pattern being formed by repeating square blocks, each block having a central square area and four side areas, the side areas being divided into smaller squares.

**15 Claims:** A scanning system for scanning a document, comprising:  
16 a) a scanner unit; b) a processing unit; c) a memory unit; d) a communication unit; e) a display unit;  
17 f) a keyboard; g) a mouse; h) a power source; i) a power switch; j) a power cord; k) a power adapter; l) a power  
18 outlet; m) a power cord connector; n) a power adapter connector; o) a power cord cable; p) a power adapter cable;  
q) a power cord cable connector; r) a power adapter cable connector; s) a power cord cable cable; t) a power adapter cable cable;  
u) a power cord cable cable connector; v) a power adapter cable cable connector; w) a power cord cable cable cable;  
x) a power adapter cable cable cable connector; y) a power cord cable cable cable connector; z) a power cord cable cable cable cable;

11. A system for scanning a document (43), said system comprising:

means (22) for illuminating the document; detector means (24, 41, 411/61, 62) for receiving light from the document and directing the light toward the detector array; and

2. A system according to claim 1; wherein the imager is telecentric.

**3. A system according to claim 1 or 2, operable to subject the document to axial (46, 46') displacement; the imager comprising an aspheric element (33), preferably at an aperture stop, for introducing spherical aberration to reduce variation (82-81-83) of resolution as a function of said axial displacement.**

4. A system according to any preceding claim, wherein the imager comprises a plurality of optical surfaces (63, 32, 33, 42, 64) in optical series (63-32-33-32-64), where the surfaces are arranged in the top-to-bottom sequence:

5. A system according to claim 4, wherein the imager comprises a diffraction pattern (33) carried by one (33) or more

the system according to claim 1, where the image comprised in the action pattern (33) can be the (33) or more of the surfaces; for correcting spectral dispersion caused by one (63) of the surfaces; and preferably the imager is telecentric with the eyepiece (40) of the instrument being used.

40 6. (A system according to claim 4 or 5, wherein the optical surfaces comprise converging mirror means (32) and a diverging mirror (33), the diverging mirror being positioned to receive light from the converging mirror means and to reflect the light toward the converging mirror means at a position of the diverging mirror and the inclusion of a third

7. A system according to claim 6, including an optical path (34-32-38/39-33-48/49-36), and wherein the reflecting mirror comprises a third mirror (40) positioned in optical coupling with the converging mirror means to fold the optical

**8. A system according to claim 6 or 7, wherein the optical axis (46, 46') of the diverging mirror is aligned with the optical axis (46, 46') of the converging mirror means.**

**9. A system according to any preceding claim, wherein the reflecting imager comprises a solid optical material. (61)**

50 and 62) defining at least one and preferably each of said plural optical surfaces as a respective internal reflective surface of the solid optical material; and (c) a cavity to which the converging mirror means

**10. A system according to any preceding claim, further comprising means (11) for translating the detector array and**

**55** **imager together across the document to obtain a signal array representing a swath (44) of the document.** It is used in commercial document scanning, and the carriage provides a mechanism for moving the imager and detector array across the document, thereby enabling the use of compact inexpensive light sources and detectors in acquiring a full page image. Nevertheless it is important to appreciate in conjunction with the other features of this invention

The isobright elevations introduced at the top of the slope; the brighter the ground, the greater the amount of light reflected by the object will be found. The result is that the object appears brighter in proportion to the level plane or circle to which it belongs. This is the principle of the isobright analysis. In this way, the observer can easily distinguish the objects in the foreground from those in the background by the relative brightness of the objects and position of angle of elevation of the object.

The maximum value of the shear stress at the center of the bottom surface is calculated for the worst-case loading condition shown in Fig. 3.3. The dimensions of the dam are given in Fig. 3.1.

The cut-off value of  $\alpha$  is determined by the condition that the sum of the expected system failure probability and the sum of the expected system repair times must be less than or equal to one. This leads to the following equation:

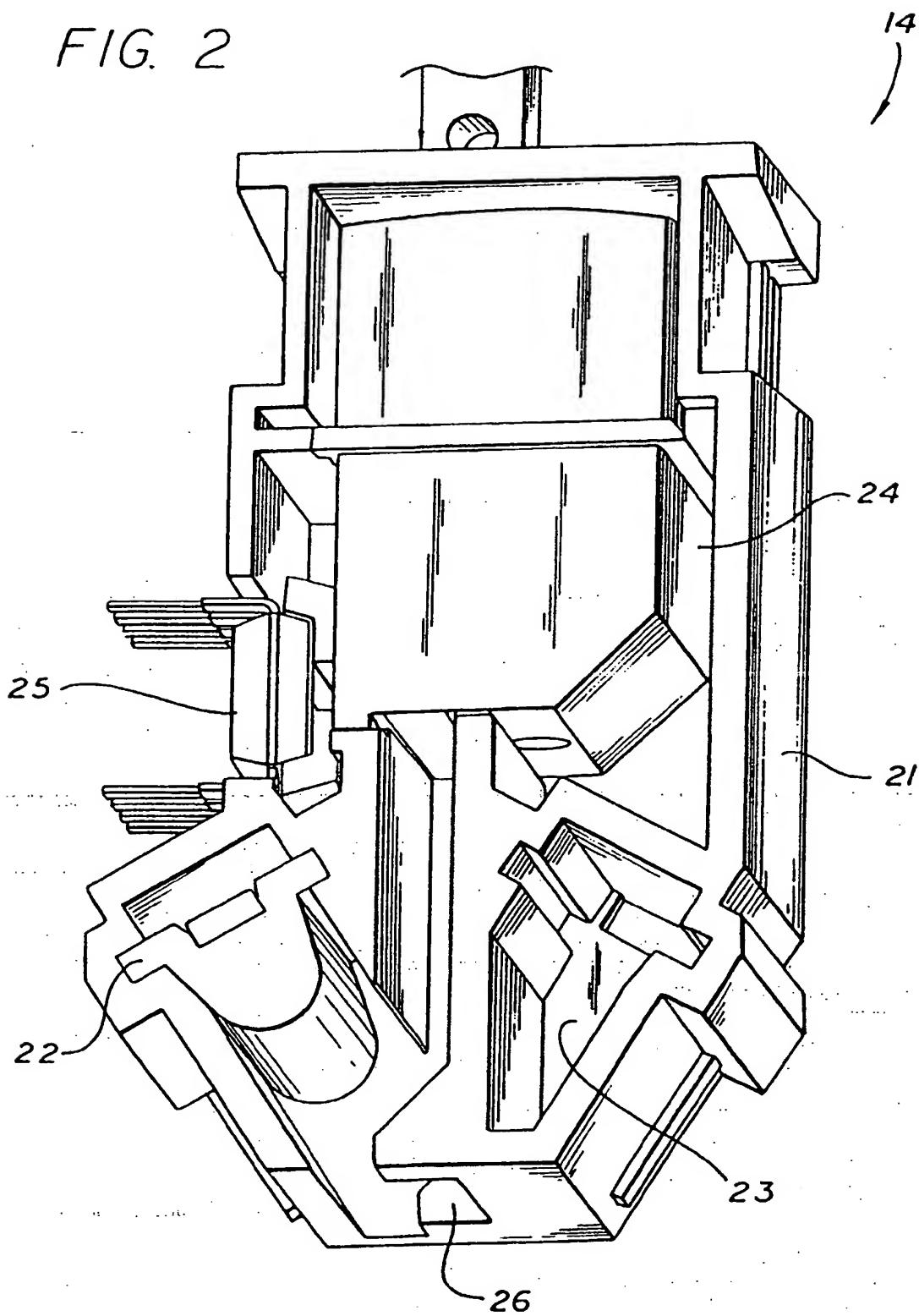
~~13. Please indicate which of the following you have had to pay for in the past year. Check as many categories as apply.~~

The following is a list of the names of the members of the 18th grade class of 1913. The names are listed in the order in which they appear in the original document.

**FIG. 3** 40 49  
Diagram illustrating the effect of the length of the fiber on the shear modulus of the material. For example, the shear modulus of a fiber of length  $L$  is denoted by  $G_L$ , where  $L$  is the length of the fiber. The shear modulus of a fiber of length  $L$  is given by  $G_L = G_0 \cdot e^{-\alpha L}$ , where  $G_0$  is the shear modulus of the fiber at zero length, and  $\alpha$  is a constant.

**FIG. 3** 40

FIG. 2



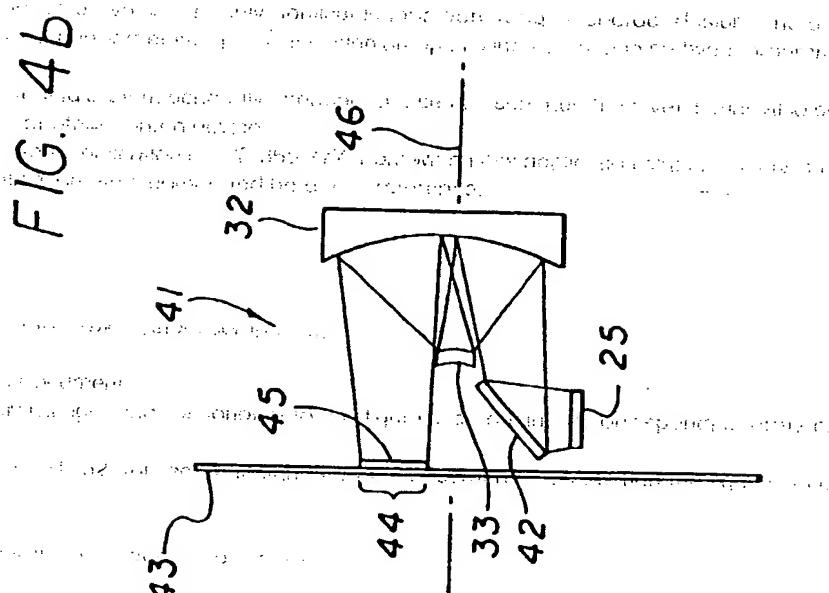
<sup>10</sup> See *U.S. v. Mink*, 490 U.S. 226, 237 (1990) (“[T]he Constitution does not prohibit Congress from enacting legislation that protects the environment.”).

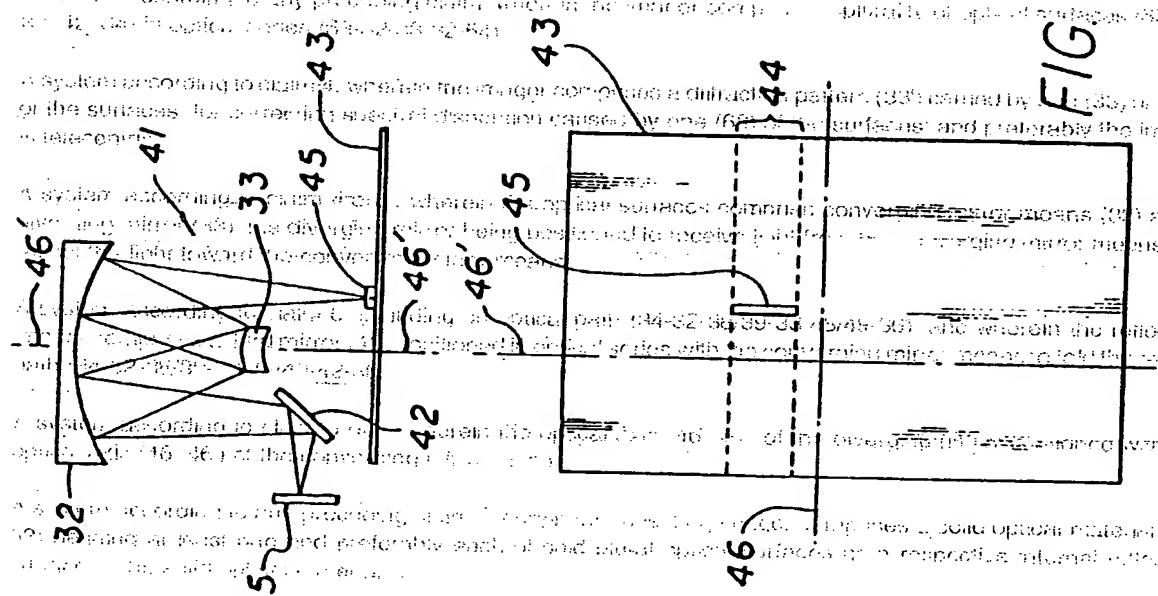
97  
The following is a list of the names of the men who were killed in the raid on the town of Cawnpore, India, on the 21st of June, 1857.

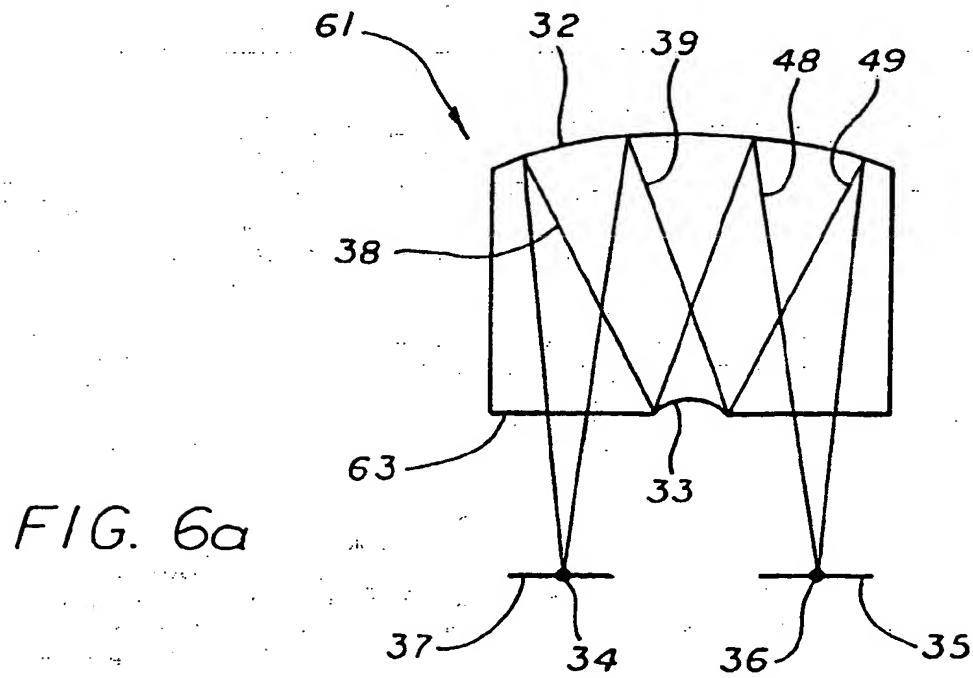
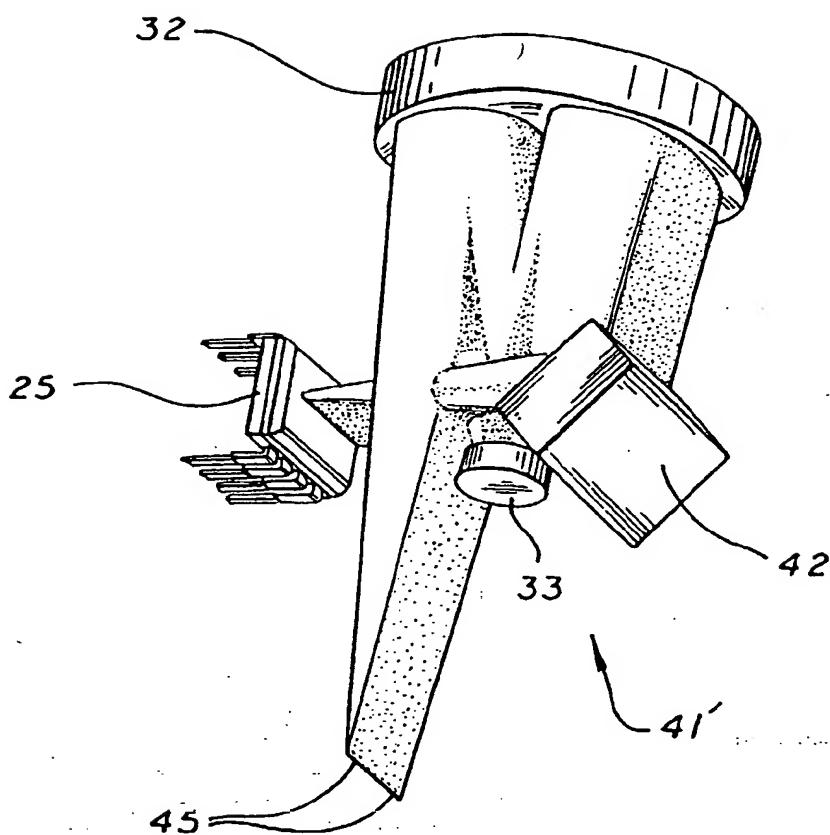
4) The following is a list of the major components of the system. The numbers correspond to the numbers in the block diagram.

*G.* The following table gives the results of the experiments made at the University of Michigan on the effect of the different factors on the rate of absorption of oxygen by the blood.

For more information about the National Institute of Child Health and Human Development, please visit the NICHD website at [www.nichd.nih.gov](http://www.nichd.nih.gov).





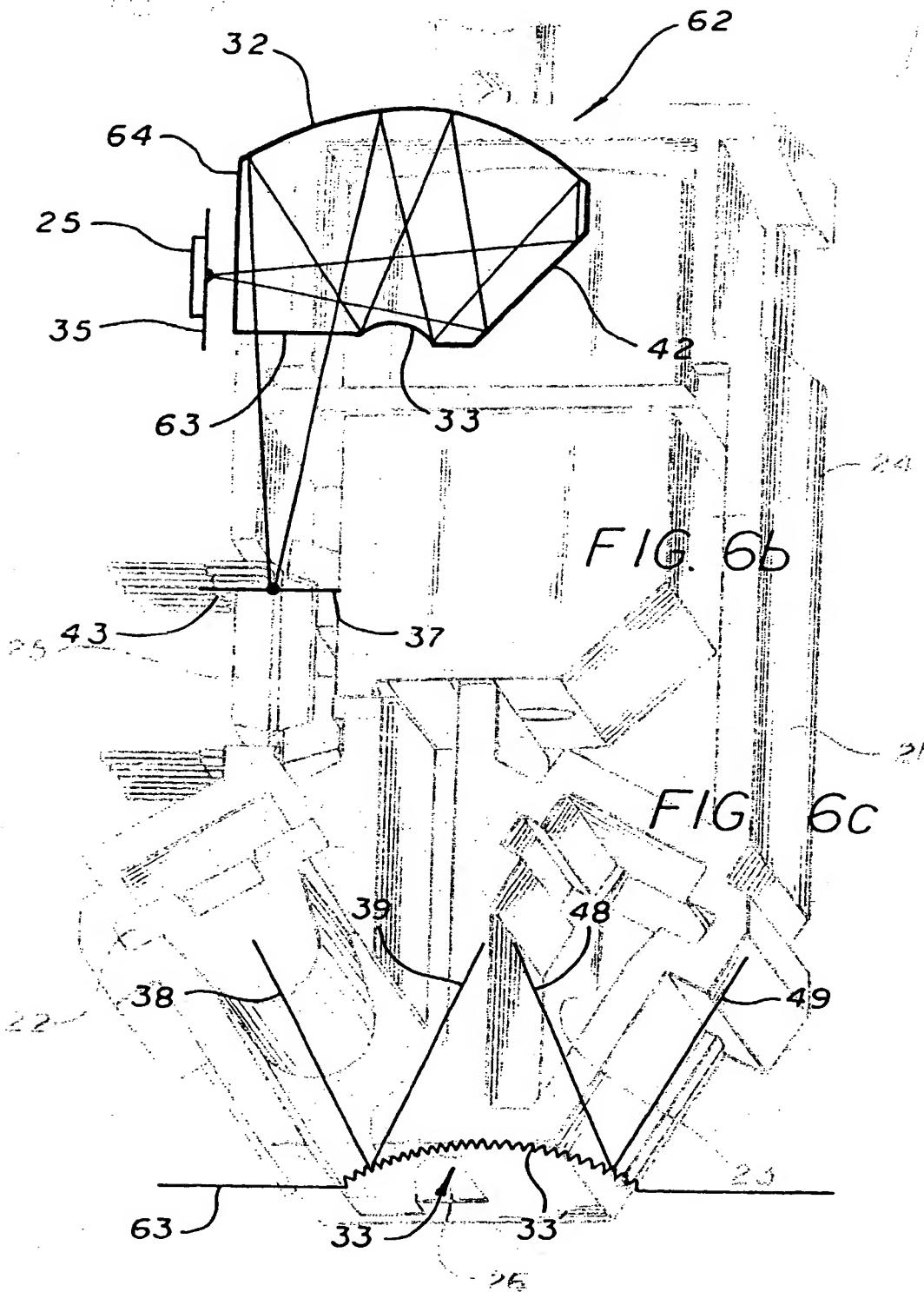
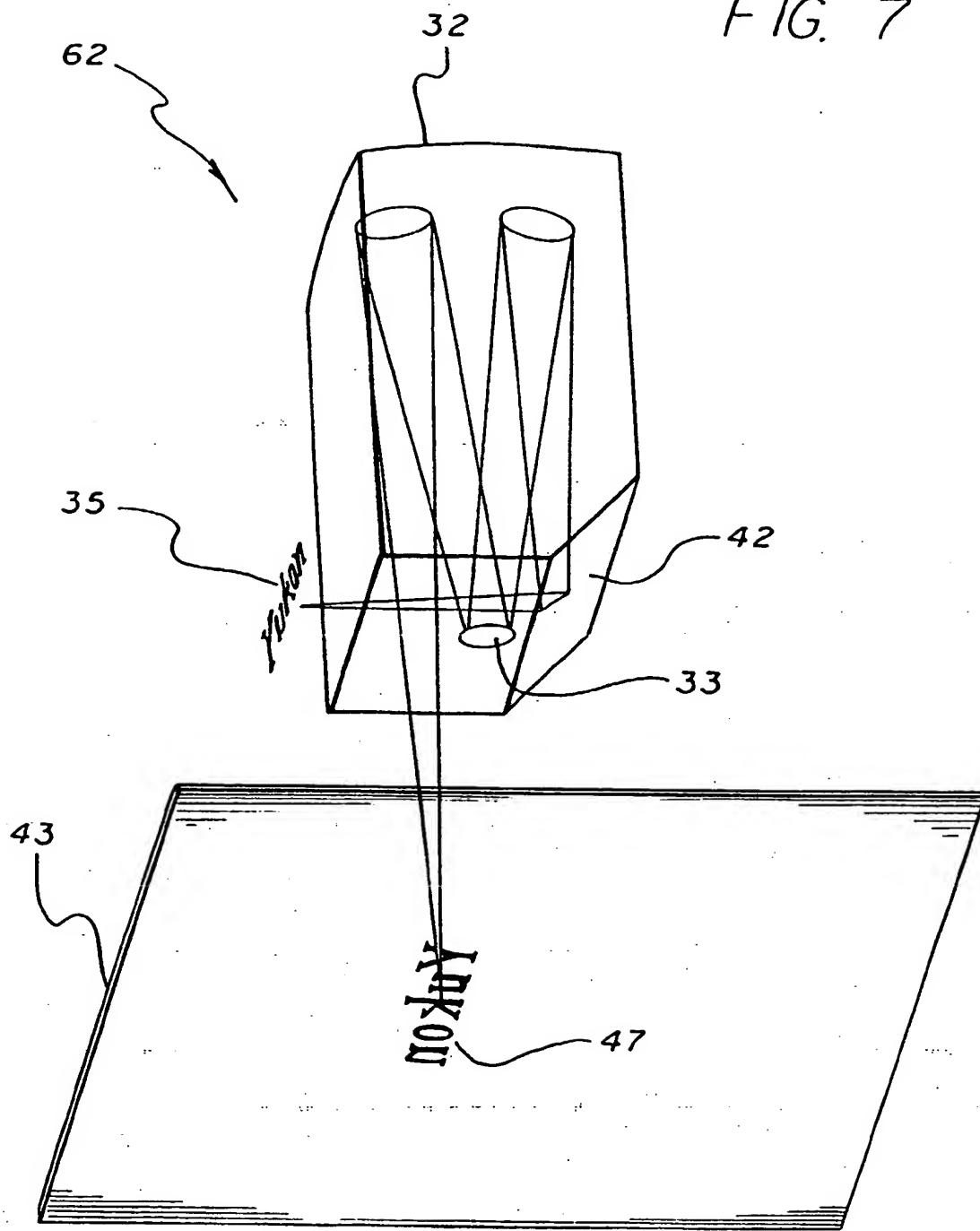


FIG. 7



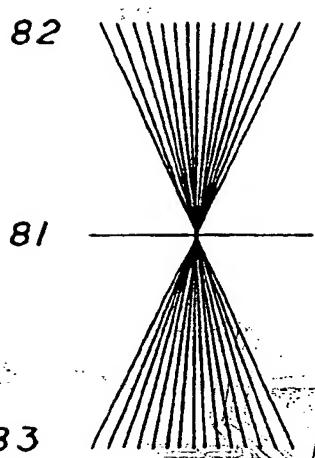


FIG. 8

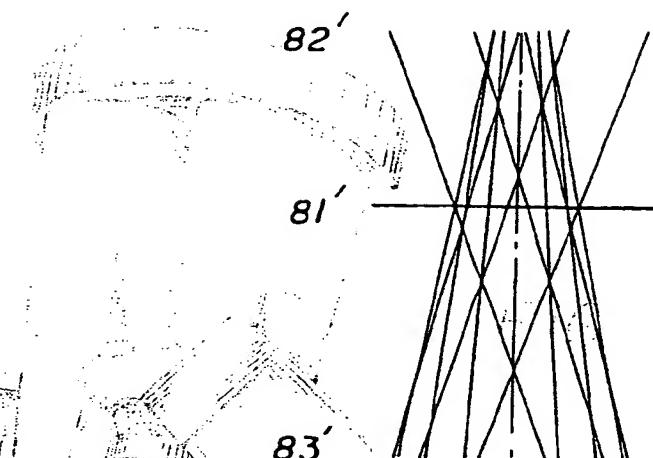


FIG. 9

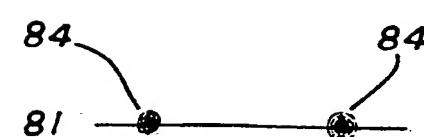
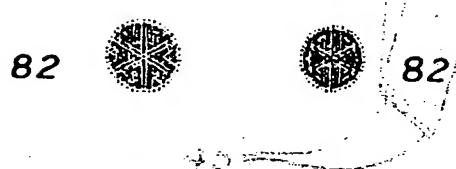


FIG. 10

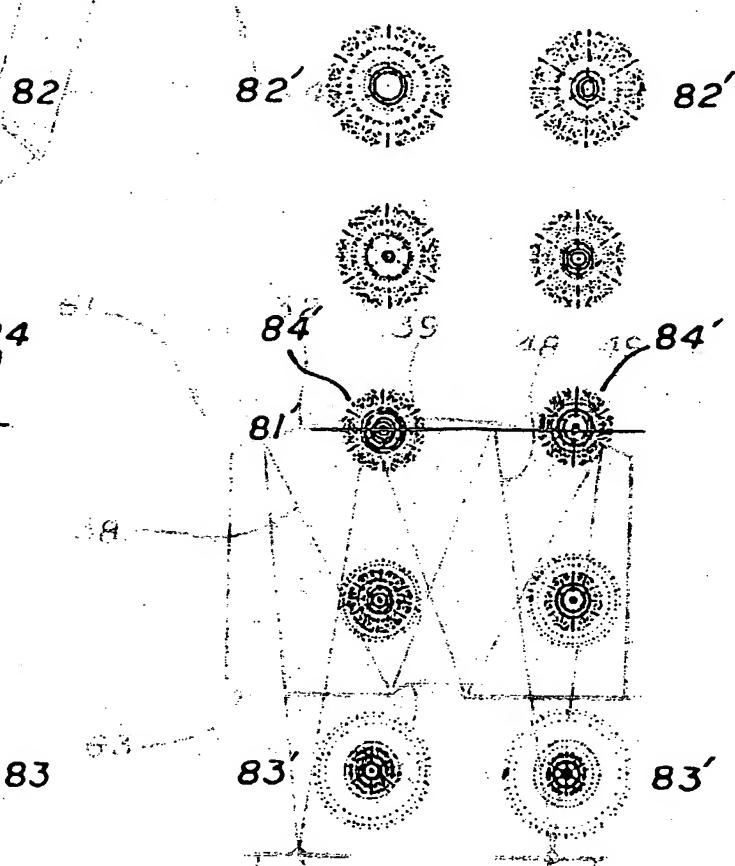


FIG. 11

FIG. 12b

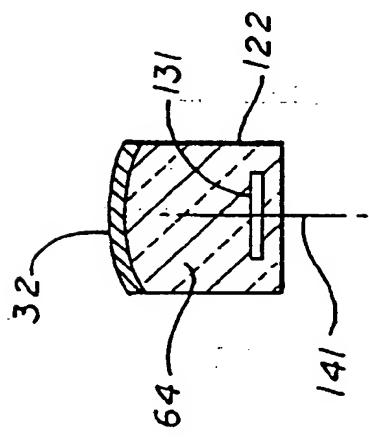


FIG. 12c

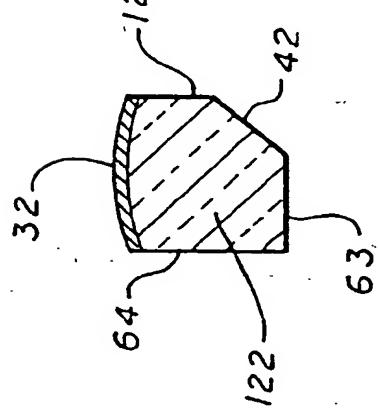


FIG. 12d

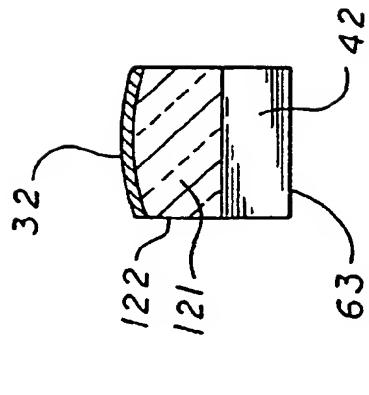


FIG. 12a

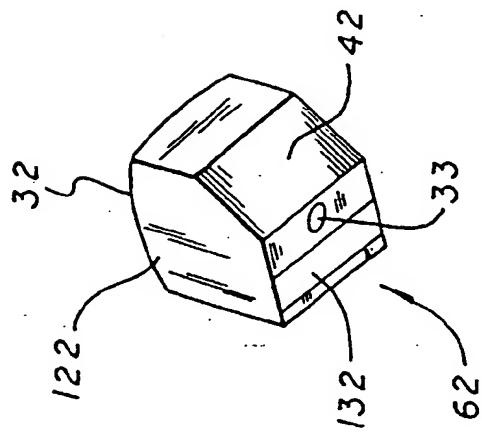
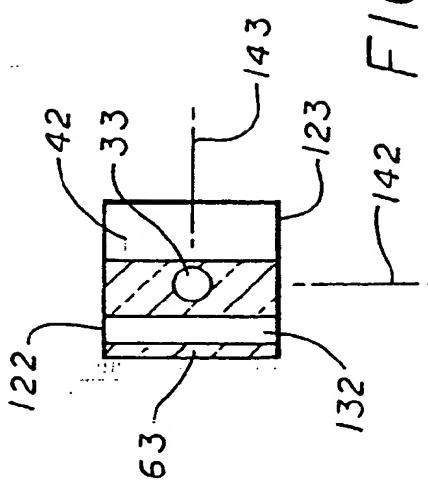


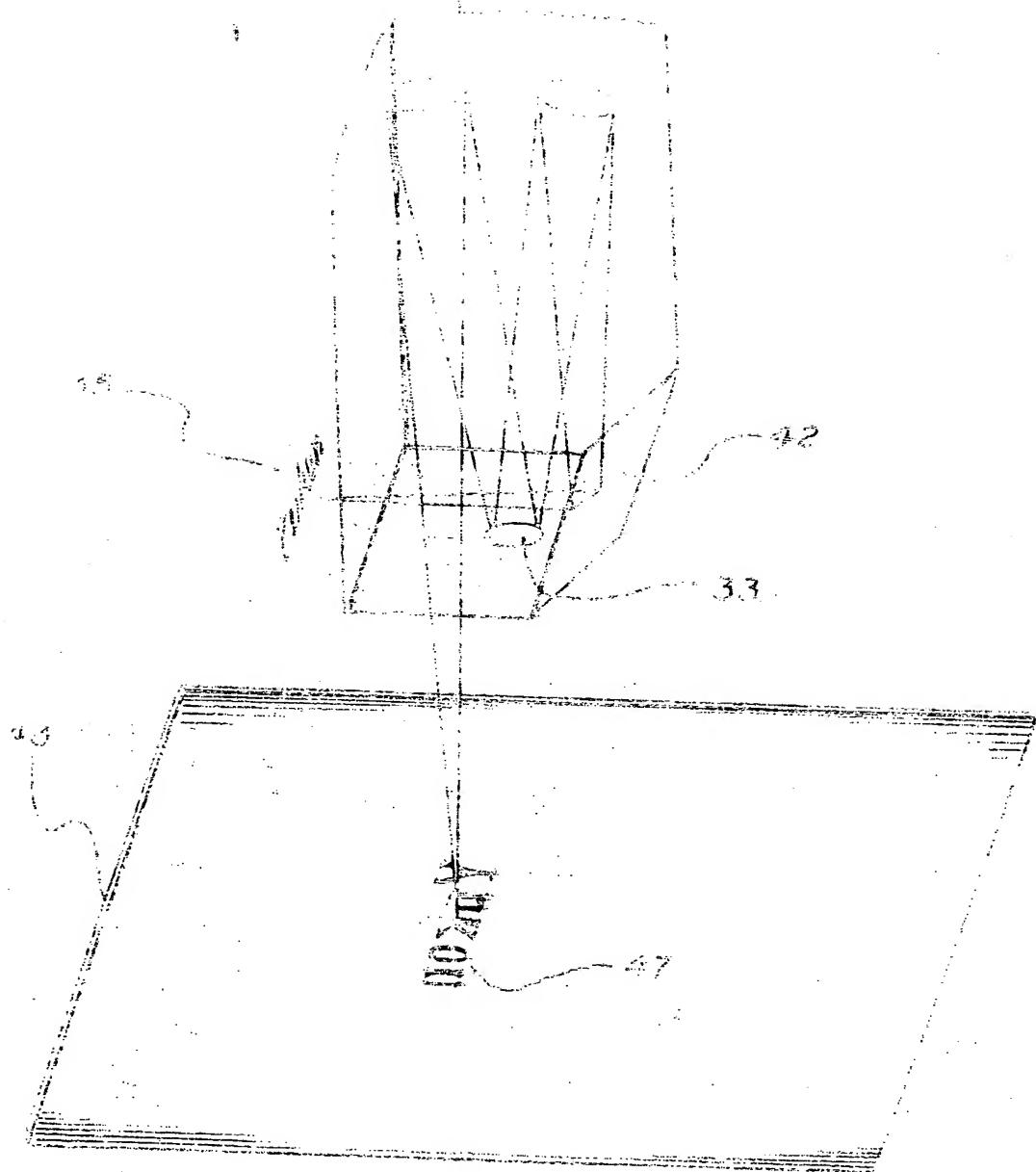
FIG. 12e



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EP 0 814 596 A3

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### (54) Scanning system

(57) In a system for scanning a document (43), a light source (22) illuminates the document; an imager (24, 41, 41', 61, 62) receives light from the document and directs it toward a detector array (25) which produces a corresponding array of electrical signals. The imager has several optical properties that are useful either individually or in combination. The imager is telecentric and thereby ensures that image size and magnification are insensitive to object displacement along the optical axis (46, 46') and image brightness is uniform independent of object off-axis distance. An aspheric element (33) within the imager balances focus variation (82-81-83)

within the depth of field with spherical aberration and thereby provide nearly uniform image resolution. A diffraction pattern (33'), carried by the imager, corrects for spectral dispersion which occurs when light passes (63) from air into a refractive material (61, 62). An imager with a reflecting surface (32, 33) provides a system that is subject to little or no chromatic aberration. A solid imager (61, 62) with multiple internal reflecting surfaces (32, 33, 42) in optical series (32-33-32-42), configured to include the previously mentioned optical properties, also provides for highly stable alignment of reflecting surfaces.

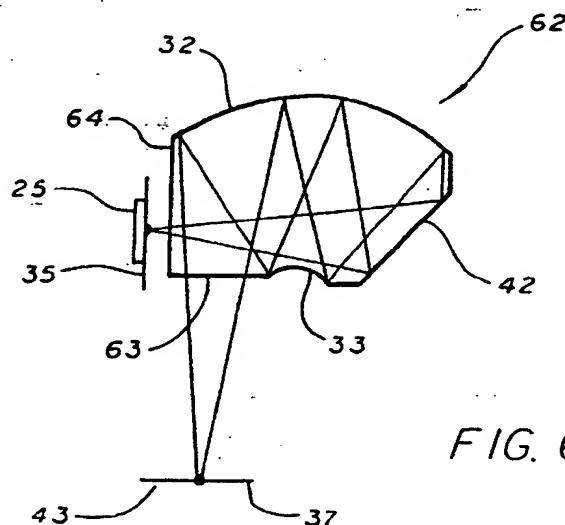


FIG. 6b



European Patent  
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## EUROPEAN SEARCH REPORT

Application Number  
EP 97 30 3844

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	GB 2 247 090 A (BARR & STROUD LTD) 19 February 1992 * the whole document *	1-4,6-8, 10	H04N1/191 H04N1/03
A	EP 0 559 370 A (CANON KK) 8 September 1993 * abstract * * figures 2,10 *	1	
A	EP 0 532 267 A (HUGHES AIRCRAFT CO) 17 March 1993 * abstract *	5	
TECHNICAL FIELDS SEARCHED (Int.Cl.6)			
H04N G02B G03B			
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
THE HAGUE	5 August 1998	Hubeau, R	
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